



## SPECIFICATION

### TITLE

**"RADIO-FREQUENCY ANTENNA FOR A MAGNETIC RESONANCE SYSTEM"**

### BACKGROUND OF THE INVENTION

#### Field of the Invention

The present invention concerns a radio-frequency antenna for a magnetic resonance system of the type having a number of antenna rods and two rings, with the antenna rods disposed regularly around an antenna axis and each connected at their respective rod ends with one of the rings and wherein either each antenna rod proceeds substantially parallel to the antenna axis and exhibits a rod spacing in a middle region of the antenna axis, or each antenna rod forms with the antenna axis an inclination angle, such that the radio-frequency antenna is in the shape of a frustrum and, at its rod end situated farther from the antenna axis, exhibits a rod spacing from the antenna axis.

#### Description of the Prior Art

Radio-frequency antennas of the above type are – in particular in the case of the antenna rods being parallel to the antenna axis – generally known as birdcage resonators. Capacitors are arranged in the rings and/or the antenna rods. The radio-frequency antenna is adjusted so that, for a predetermined or predeterminable operating frequency of the radio-frequency antenna, it forms a resonant oscillating circuit.

Birdcage resonators are known from German PS 197 32 783 and Patent Abstracts of Japan for JP-A-2000 166 895, in which the rings are farther from the antenna axis than the antenna rods.

Nuclear spins of an examination subject (often a person) are excited to resonance by magnetic fields emitted by such radio-frequency antenna. The

resonances are then acquired and evaluated. The acquisition of the resonance signals can ensue with the same antenna.

Due to the trend toward ever-shorter magnet systems, the risk exists in conventional whole-body transmitting antennas that an image artifact known as the ambiguity artifact will occur. Ambiguity artifacts are caused by, due to the superimposition of basic magnetic field and gradient magnetic field, two or more locations existing at which the same total field strength predominates. Typically, one of these locations is situated within a desired acquisition volume, and at least one further location is situated outside of the acquisition volume. If the radio-frequency field strength at the location outside of the acquisition volume is of a sufficient volume, it leads to the superimposition of the image information from both locations in the image reconstruction.

To prevent the ambiguity artifact, it must be insured that the radio-frequency magnetic field outside of the acquisition volume decreases sufficiently rapidly. It must simultaneously be insured for that the radio-frequency signal is sufficiently homogenous within the acquisition volume.

Whole-body transmitting antennas normally are fashioned as birdcage resonators. Due to this design, these antennas already possess a rapid field drop-off in the lengthwise (longitudinal) axis, however, severe limitations in the field homogeneity arise in the case of very short magnets and/or very short antennas.

From the scientific essay "Fast drop off cylindrical Radio-frequency transmit coils", by E. B. Boskamp, appearing in the Proceedings of the ISMRM volume 10 (2002), a combination of a number of birdcage resonators is specified that are connected with one another such that a suitable field profile can be generated.

A radio-frequency antenna for a magnetic resonance system is known from United States Patent No. 6,344,745 that has a number of antenna rods and two rings. In this radio-frequency antenna, the antenna rods are regularly arranged around an antenna axis and are connected at their rod ends with one of the rings per rod end. Each antenna rod is substantially parallel to the antenna axis and exhibits in a middle region a rod spacing from the antenna axis that is larger than a ring spacing from the antenna axis for at least one of the rings in the region of this antenna rod. In this radio-frequency antenna, the antenna rods gradually proceed radially inwardly over an area that amounts to at least 37.5 % of the total length of the antenna rods. In this area, the antenna rods are curved radially inwardly in the shape of a circular arc. This area extends to the end of the respective antenna rod.

A radio-frequency antenna for a magnetic resonance system is known from German OS 100 52 192 that has a number of antenna rods and two rings. In this radio-frequency antenna, the antenna rods also are regularly arranged around an antenna axis and also are connected at their rod ends with one of the rings per rod end. The antenna rods also are substantially parallel to the antenna axis and exhibit in a middle region a rod spacing from the antenna axis that is larger than a ring spacing from the antenna axis for at least one of the rings in the region of this antenna rod. This is achieved by the antenna rods being curved over their entire length, such that the radio-frequency antenna has a barrel-like appearance.

Various radio-frequency antennas for a magnetic resonance system are known from Japanese Application 2001 145 608. In these radio-frequency antennas, a number of antenna rods are regularly arranged around an antenna axis. The antenna rods are connected at their rod ends with rings. In one of these radio-frequency antennas, the antenna rods, relative to the antenna axis, form an

inclination angle, such that the radio-frequency antenna is fashioned in the shape of a frustrum. At the rod ends situated farther from the antenna axis, the antenna rods exhibit a rod spacing from the antenna axis. At this location, the ring appears to exhibit the same spacing from the antenna axis as the respective antenna rod.

A radio-frequency antenna for a magnetic resonance system is known from United States Patent No. 4,736,161 that has a number of antenna rods and two rings. In this radio-frequency antenna, exactly two detuning circuits are present by means of which the radio-frequency antenna can be detuned. The detuning circuits are connected to supply cables for the radio-frequency antenna. A similar arrangement is described in European Application 0 758 091.

A radio-frequency antenna for a magnetic resonance system is known from United States Patent Application Publication No. 2002/0011843 that has a number of antenna rods and two rings, wherein the antenna rods form two substructures twisted opposite one another, each of the substructures being regularly arranged around the antenna axis, and the substructures exhibiting rod spacings differing from one another. The substructures are thereby arranged in a circular fashion around the antenna axis.

### **SUMMARY OF THE INVENTION**

An object of the present invention is to provide a radio-frequency antenna suitable for magnetic resonance systems, with which a faster outward field drop-off can be achieved in a simple manner.

The above object is achieved in a radio-frequency antenna of the initially cited type having antenna rods parallel to the antenna axis, wherein the rod spacing from the antenna axis is larger than a ring spacing from the antenna axis for at least one of the rings in the region of this antenna rod, and wherein this is accomplished by

either the antenna rods, with regard to their total length, being bent radially inwardly only in the area of the longitudinally outermost 10 %, or the antenna rods, with regard to their total length, proceed radially inwardly from their middle region over at least 20 %, and in the longitudinally outermost 10 % do not exhibit radially inward charge, or the rings, at regions at which the rods are connected, are directed radially outwardly towards the antenna rods.

The above object also is achieved in a radio-frequency antenna of the initially cited type having an inclination angle between the antenna rods and the antenna axis, wherein the rod spacing from the antenna axis is larger than a ring spacing from the antenna axis for at least one of the rings in the region of this antenna rod, by means of the rod end of this antenna rod being situated farther from the antenna axis than the ring.

The connection of the antenna rods with the ring can in this case in particular be effected by the antenna rods being directed radially inwardly at the appertaining rod end. Alternatively, it is possible for the connection of the antenna rods with the one ring or the rings to be effected by the appertaining ring being directed radially outwardly to the antenna rods in its connection region.

The inventive effect is stronger the smaller that the ring spacing is compared than the rod spacing. The difference between the ring spacing and the rod spacing should be at least 5 mm (preferably 10 to 15 mm).

The antenna rods and the rings preferably are radially outwardly surrounded by a radio-frequency shielding.

As a rule, the radio-frequency shielding has in the region of the antenna rod in question, a shielding spacing from the antenna axis. A particularly good effect results from the reduction of the ring spacing when the difference between the ring

spacing and the rod spacing is at least 15 % (preferably 20 % to 40 %) of the difference between the shielding spacing and the rod spacing.

The radio-frequency shielding optionally can be arranged symmetrically or asymmetrically with regard to the antenna axis.

By reducing the spacing of the appartaining ring to the antenna axis compared to that of the antenna rods, the outlay for detuning the radio-frequency antenna also can be reduced. It is in particular sufficient when the radio-frequency antenna has exactly two detuning circuits with which the radio-frequency antenna can be detuned.

Conventionally, the detuning circuits are installed in the radio-frequency antenna itself, in particular they are arranged in the connection regions of the rings with the antenna rods. In contrast, in the inventive radio-frequency antenna it is possible for the detuning circuits to be connected to supply cables for the radio-frequency antenna.

When the radio-frequency antenna is externally installed on a carrier tube, the designed arrangement of the individual components of the radio-frequency antenna can be realized in a particularly simple manner.

The inventive radio-frequency antenna can be fashioned as a local antenna or as a whole-body antenna. In particular in the latter case, the rod spacing is typically between 25 and 35 cm.

In an even further optimized embodiment, the antenna rods can form at least two substructures that are circumferentially rotated (offset) relative to one another, with each of the substructures being regularly arranged around the antenna axis and the substructures exhibiting rod spacings differing from one another. The antenna

rods or the substructures are as a rule arranged circularly around the antenna axis, however, they can also be arranged elliptically around the antenna axis.

The rings are as a rule arranged symmetrically with regard to the antenna axis, however, they can also be arranged asymmetrically with regard to the antenna axis.

### **DESCRIPTION OF THE DRAWINGS**

FIG... 1 schematically illustrates the basic components of a magnetic resonance system in which the inventive radio-frequency antenna can be used.

FIG... 2 shows a known radio-frequency antenna in a perspective view.

FIG.. 3 shows the radio-frequency antenna of FIG.. 2 in a plan view.

FIG.. 4 shows the radio-frequency antenna of FIG.. 2 from the side.

FIG.. 5 shows the radio-frequency antenna of FIG.. 2 in unrolled representation.

FIG.. 6 illustrates a first embodiment of a connection between a ring and the antenna rods in a radio-frequency antenna in accordance with the invention.

FIG.. 7 illustrates a second embodiment of a connection between a ring and the antenna rods in a radio-frequency antenna in accordance with the invention.

FIG.. 8 is a side schematic view of a first embodiment of an antenna rod in a radio-frequency antenna in accordance with the invention.

FIG.. 9 is a side schematic view of a second embodiment of an antenna rod in a radio-frequency antenna in accordance with the invention.

FIG.. 10 is a plan view of a further embodiment of a radio-frequency antenna in accordance with the invention.

FIG.. 11 is a side view of a radio-frequency antenna in accordance with the invention, in a frustrum embodiment.

FIG.. 12 is a plan view of an elliptically shaped embodiment of a radio-frequency antenna in accordance with the invention.

FIG.. 13 is a plan view of a further embodiment for arranging the antenna rods relative to the antenna axis in accordance with the invention.

FIG.. 14 is a further elliptically shaped embodiment of a radio-frequency antenna in accordance with the invention.

### **DESCRIPTION OF THE PREFERRED EMBODIMENTS**

As shown in FIG. 1, a magnetic resonance system has an examination space 1. A patient 3 (in general: an examination subject 3) can be inserted into the examination space 1 by means of a patient bed 2. The examination space normally is substantially cylindrically and exhibits an inner diameter D.

The examination space 1 is surrounded by various magnets and magnet systems. The first is a basic field magnet 4. The basic field magnet 4 serves to generate a homogenous basic magnetic field. A gradient magnet system 5 is also present. Gradient fields are generated by means of the gradient magnet system 5 that are necessary for the generation of meaningful, evaluable magnetic resonance signals. The magnet system also has a whole-body coil 6. The whole-body coil 6 is fashioned as a radio-frequency antenna. In operation, it serves as a transmitting antenna to excite magnetic resonance signals in the examination subject 3. In operation as a receiving antenna, it serves to receive the excited magnetic resonance signals of the examination subject 3.

At least one local coil 7 normally can be inserted inside the examination space 1. It is likewise fashioned as a radio-frequency antenna. It normally serves for local reception of magnetic resonance signals that have been previously excited by means of the whole-body coil 6, however, in the individual case the local coil 7, like



the whole-body coil 6, also can be operated as a transmitting antenna. The design of the local coil 7 can – except for correspondingly smaller dimensions – be similar to the design of the whole-body coil 6.

The basic field magnet 4, the gradient field magnet system 5 and the coils 6, 7 are surrounded by a shielding magnet 8.

The gradient magnet system 5 and the coils 6, 7 are connected to a control and evaluation unit 9 for suitable control of the gradient magnet system 5 and of the coils 6, 7 in a known manner to excite, to receive and to evaluate magnetic resonance signals.

As shown in FIG. 2, a conventional radio-frequency antenna 6, 7 – be it in the form of the whole-body coil 6, be it in the form of the local coil 7 – has a number of antenna rods 10 as well as two rings 11. Also arranged in the antenna rods 10 and/or the rings 11 are capacitors C by means of which the radio-frequency antenna 6, 7 is tuned to a specific operating frequency. These capacitors C are arranged in the rings 11 according to FIG. 2. The rings 11 thus have ring segments, however, this is of secondary importance in the framework of the present invention.

The antenna rods 10 in the embodiment according to FIG. 2 are parallel to an antenna axis 12. They are arranged at a rod spacing  $d_s$  from the antenna axis, uniformly distributed around the antenna axis 12. The rod spacing  $d_s$  is the same for all antenna rods.

In the case of the whole-body coil 6, the rod spacing  $d_s$  is minimally larger than half of the diameter D of the examination space 1. The rod spacing  $d_s$  typically ranges between 25 and 35 cm. Give fashioning of the radio-frequency antenna as a local coil 7, the rod spacing  $d_s$  can naturally be smaller than 25 cm.

The antenna rods 10 are connected to the respective rings 11 at their rod ends E (see FIG. 8 and 9). The rings 11 are thus arranged concentric to the antenna axis 12.

The rings 11 each exhibit ring spacing  $d_r$  from the antenna axis 12 that are smaller than the rod spacing  $d_s$ . According to FIG. 3, the ring spacing  $d_r$  of each ring 11 is smaller than the rod spacing  $d_s$ . In principle, however, it would be sufficient for only the ring spacing  $d_r$  for only one ring 11 to be smaller than the rod spacing  $d_s$ . The ring spacing  $d_r$  preferably is at least 5 mm (more preferably 10 to 15 mm) smaller than the rod spacing  $d_s$ .

As can be seen from FIG. 3, the antenna rods 10 and the rings 11 are radially, externally surrounded by a radio-frequency shielding 13. The radio-frequency shielding 13 proceeds concentrically around the antenna axis at a shielding spacing  $d_S$ . The radio-frequency shielding 13 thus always exhibits the same shielding spacing  $d_S$  from the antenna axis 12 in the region of the antenna rods 10. The difference of the shielding spacing  $d_S$  and the rod spacing  $d_s$  is typically between 25 and 35 mm, for example 30 mm. The difference of the ring spacing  $d_r$  and the rod spacing  $d_s$  should be at least 15 % (preferably 20 to 40 %) of the difference between the shielding spacing  $d_S$  and the rod spacing  $d_s$ . Given a spacing of the radio-frequency shielding 13 from the antenna rods 10 of 25/30/35 mm, the radial spacing of the rings 11 from the antenna rods 10 is thus at least 2.75/4.50/5.25 mm (preferably 5/6/7 to 10/12/14).

As can be seen particularly clearly from FIG. 3 and 4, the antenna rods 10 and the rings 11 are externally mounted on a carrier tube 14 (here cylindrical). In the case of the whole-body coil 6, the carrier tube 14 corresponds to the inner wall of the examination space 1. The increased spacing of the antenna rods 10 from the rod

axis 12 can be ensured by a separate spacer 15 placed on the carrier tube 14. The spacer 15 preferably is formed of a thermally insulating material, for example polyurethane foam.

According to FIG. 5, the radio-frequency antenna 6, 7 has exactly two detuning circuits 16 that are connected to supply cables 17 for the radio-frequency antenna 6 or 7. The detuning circuits 16, for example, are fashioned as capacitor networks that can be switched on via diode switches on the supply cables 17. By switching on the detuning circuits 16 on the supply cables 17, a detuning of the radio-frequency antenna 6 or 7 is thus possible.

According to FIG. 6, the connection of the antenna rods 10 with the rings 11 is effected by the antenna rods 10 being directed radially inwardly toward their rod ends E. Alternatively, however, it is possible according to FIG. 7 for the connection of the antenna rods 10 with the rings 11 to be effected by the rings 11 projecting radially outwardly at their connection regions to the antenna rods 10.

When the antenna rods are directed inwardly toward their rod ends E, this can be realized in two manners that can be used alternatively. As shown in FIG. 8 the antenna rods 10 in the region of the rod ends E are bent radially inwardly. In this case, the bending ensues, with regard to the total length of the antenna rods 10, in the last 10 %, in particular in the last 5 %, before the rod end E. According to FIG. 9, however, it is also possible for the antenna rods 10 to gradually proceed radially inwardly from the middle region M to the rod ends E. The gradual, radially inward course extends in this case over at least 20 % (preferably 30 to 35 %) of the total length of the antenna rods 10. In this case, preferably no further radial spacing change ensues in the outermost 10 % of the antenna rod 10.

In each of the embodiment described above (compare in particular the representations in FIG. 2, 8 and 9) each antenna rod 10 proceeds substantially parallel to the antenna axis 12. In its middle region M, it exhibits the rod spacing  $d_s$  from the antenna axis 12. This rod spacing  $d_s$  is longer than the ring spacing  $d_r$  from the antenna axis 12 that the rings 11 exhibit.

As shown in FIG. 2 and 3, and as assumed in connection with FIG. 8 and 9, the antenna rods 10 normally are arranged circularly around the antenna axis 12. The rings 11 and the radio-frequency shielding 13 also are normally arranged symmetrically relative to the antenna axis 12. As shown in FIG. 10, however, it is also possible for one of the rings 11 (or both rings 11) and/or the radio-frequency shielding 13 to be arranged asymmetrically with regard to the antenna axis 12. A possible asymmetric arrangement of the radio-frequency shielding 13 can be realized independent of an asymmetric arrangement of one of the rings 11 or, respectively, of both rings 11.

According to FIG. 11, it is furthermore possible to fashion the radio-frequency antenna not in the shape of a cylinder, but rather in the shape of a frustrum.. In this case, the antenna rods 10, together with the antenna axis 12, form an inclination angle  $\alpha$ . Corresponding to this, each antenna rod 10 has a rod end E that is situated farther from the antenna axis 12 than the other rod end E. The rod spacing  $d_s$  is in this case the spacing from the antenna axis 12 of this rod end E (thus of the rod end E situated farther from the antenna axis 12). This rod spacing  $d_s$  is in this case greater than the ring spacing  $d_r$  from the antenna axis 12 of the ring 11 that is connected with this rod end E.

As shown in FIG. 12, the arrangement of the antenna rods 10 also is not necessarily circular. Rather, it is sufficient for the antenna rods 10 to be regularly

arranged around the antenna axis 12. For example, the antenna rods 10, as shown FIG. 12, can be arranged elliptically around the antenna axis 12. Local fields can thereby be generated, for example in the shoulder region of the patient 3, that are smaller in extent than in the breast or back region of the patient 3. The occupancy ratio of the antenna can be increased without increasing the stress on the patient 3.

It is also possible, as shown in FIG. 13, for the antenna rods 10 to form two substructures rotated oppositely to one another with regard to the antenna axis 12. In this case, each of the substructures 10', 10'' is regularly arranged around the antenna axis 12. The substructures 10', 10'' in this case exhibit rod spacings  $ds'$ ,  $ds''$  that are different from one another. They preferably are arranged on gaps relative to one another.

In the embodiment of FIG. 13, the substructures 10', 10'' are arranged circularly around the antenna axis 12, however, here as well a regular arrangement is sufficient. In particular, an elliptical arrangement (see FIG. 14) is again possible.

The goals according to the object can be achieved in a simple manner by the inventive radio-frequency antenna, without impairment of the homogeneity of the generated radio-frequency field.

Although modifications and changes may be suggested by those skilled in the art, it is the intention of the inventor to embody within the patent warranted hereon all changes and modifications as reasonably and properly come within the scope of his contribution to the art.